



LOADING RESPONSE OF DENSELY PACKED PARTICLE ASSEMBLIES IN FLUID

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OBJECTIVE

Understanding mechanical properties of granular media in fluid, such as saturated soils, submerged road foundations, or flooded track ballasts, is of a great benefit in the design of transportation systems. The objective of this research is to couple the Discrete Element Method (DEM) and Lattice **Boltzmann Method (LBM) in order to accurately simulate mechanical** properties of closely packed particle assemblies in fluids.

CURRENT STATE

- Implemented parallel LBM flow module
- Calculated force and torque exerted by fluid on spherical particles
- Validated LBM module through test cases
- **Coupled LBM module with a DEM code**
- Validated a coupled system with reference simulations including:
- Drafting-Kissing-Tumbling

RESULTS

http://www.cavs.msstate.edu/projects/dem_lbm



- Large Scale Sedimentation Case
- **Initial simulations of biaxial (2D) loading of un-drained granular media**

(1)

(2)

(6)

LBM THEORY

LBM density distribution functions

The macroscopic fluid density ρ at each lattice point is a sum of the distribution functions at that lattice point:

$$\rho = \sum_{i=0}^{14} f_i$$

Fluid velocity is a weighted sum of lattice velocities:



Equilibrium

For the D3Q15 lattice, the equilibrium distribution function f_i^{eq} , given the macroscopic velocity $\boldsymbol{u}(\boldsymbol{r})$ and density $\rho(\boldsymbol{r})$, is:

$$f_i^{\text{eq}}(\boldsymbol{r}) = w_i \rho(\boldsymbol{r}) \left(1 + 3 \frac{\boldsymbol{e}_i \cdot \boldsymbol{u}(\boldsymbol{r})}{c^2} + \frac{9}{2} \frac{(\boldsymbol{e}_i \cdot \boldsymbol{u}(\boldsymbol{r}))^2}{c^4} - \frac{3}{2} \frac{\boldsymbol{u}(\boldsymbol{r}) \cdot \boldsymbol{u}(\boldsymbol{r})}{c^2} \right),$$
(5)

with the lattice velocity $c = \Delta x / \Delta t$ and the weights

$$v_i = \begin{cases} 4/9 & i = 0\\ 1/9 & i = 1, 2, 3, 4\\ 1/36 & i = 5, 6, 7, 8. \end{cases}$$

Time evolution of the distribution functions

Using the collision model of Bhatnagar-Gross-Krook (BGK) with a single relaxation time, evolution of the distribution functions is

$$f_{i}(\boldsymbol{r} + \boldsymbol{e}_{i}\Delta t, t + \Delta t) = f_{i}(\boldsymbol{r}, t) + \frac{1}{\tau_{u}} \left(f_{i}^{eq}(\boldsymbol{r}, t) - f_{i}(\boldsymbol{r}, t) \right), i = 0 \dots 8$$
(3)

 Δt ... time step

- r ... space position of a lattice site
- $t \dots$ time position of a lattice site
- $\tau_{\rm u}$... relaxation parameter for the fluid flow.

Viscosity

The relaxation parameter τ_{u} specifies how fast each particle distribution function f_i approaches its equilibrium f_i^{eq} . Kinematic viscosity ν is related to the relaxation parameter $\tau_{\rm u}$, the lattice spacing Δx , and the simulation time step Δt by

$$\nu = \frac{\tau_{\rm u} - 0.5}{3} \frac{\Delta x^2}{\Delta t}.$$

Depending on the dimensionality d of the modeling space and a chosen set of the discrete velocities e_i , the corresponding equilibrium particle distribution function can be found.

Color represents vertical component of force on particles upon compaction

SEDIMENTATION

(4)



